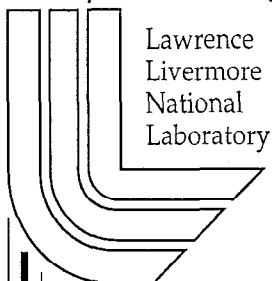


Modeling of Steel Spheres Impacting Polyethylene

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Modeling of Steel Spheres Impacting Polyethylene

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Introduction

The effect of shrapnel on target chamber components and experiments at large lasers such as the National Ignition Facility at LLNL and the Megajoule Laser at CESTA in France is an important issue in fielding targets and exposure samples. Modeling calculations are likely to be an important component of this effort. Some work in this area has been performed by French workers, who are collaborating with the LLNL on many issues relating to target chamber, experiment-component, and diagnostics survival.

Experiments have been performed at the Phébus laser in France to measure shrapnel produced by laser-driven targets; among these shots were experiments that accelerated spheres of a size characteristic of some of the more damaging shrapnel. These spheres were stopped in polyethylene witness plates. The penetration depth is characteristic of the velocity of the shrapnel. Experimental calibration of steel sphere penetration into polyethylene was performed at the CESTA facility. The penetration depth has been reported (ref. 1) and comparisons with modeling calculations have been made (ref. 2). There was interest in a comparison study of the modeling of these experiments to provide independent checks of the calculations. This work has been approved both by DOE headquarters and by the French Atomic Energy Commission (CEA); it is task number 99-3.2 of the 1999 ICF agreement between the DOE and the CEA. Daniel Gogny of the CEA who is on a long-term assignment to LLNL catalyzed this collaboration. This report contains the initial results of our modeling effort.

Modeling

Our first task was to reproduce, to the extent possible, Alain Geille's modeling (ref. 2) of the problem. To this end, we used the CALE 2-D axisymmetric code (ref. 3) run in an Eulerian mode. Zoning was uniform along the direction of the projectile velocity vector which is in the axial direction in the model. In the radial direction, uniform zoning was maintained out to 1 mm which was several projectile radii. Further out, radial zone size was increased by constant ratios of up to 1:1.05. A representative initial setup is

presented in fig. 1 with zoning shown in the lower half. Zoning was chosen so that the projectile covers ~20 zones in the axial direction and a few more zones in the radial direction.

First Calculations using CEA-style material models:

Among the material models available to us, we selected those that matched, as closely as possible, the ones reported by the French modelers. The parameters of our model are listed in Table 1. The polyethylene elastic modulus and yield strength have been derived by French workers from experiments they conducted.

Our penetration results for steel spheres into polyethylene witness plates that used the French material properties are presented in Figures 2 through 5. The calculated penetration depth is compared to Geille's results (ref. 2) in Table 2. Our calculated penetrations exceed those of Geille in all cases but are not radically different. The shape of the projectile after it comes to rest is quite similar to that reported (ref. 2) except at the lowest incident velocity. At that velocity, our projectile shows hardly any of the flattening that is present in the French modeling. The recovered projectiles exhibited less deformation than the calculated shapes (refs. 2,4). Our computed penetration depths are compared with the French experimental data in fig. 6. It is evident that the computed depths exceed the experimental values.

Second Calculations using modified material models:

We then examined the effect of changes in the material parameters. The stainless-steel projectiles used in the experiments have not yet been characterized. We chose to model them with a Steinberg-Guinan constitutive model for stainless steel (ref. 5). This steel has the lowest yield strength of the few for which a Steinberg-Guinan model has been developed. We also changed the Gruneisen equation of state to that of 304 stainless steel. Furthermore, we decreased the spall strength of the polyethylene from 20 kbars to 2 kbars, which we deem to be a more reasonable value. The material-model parameters for this set of calculations are presented in table 3. These changes decreased the calculated penetration depths as well as the projectile deformation. By itself, the reduction on the polyethylene spall strength increases the calculated penetration depth by a few percent. Finally, we increased the yield strength of the polyethylene to 1.5 kbars. The results of these calculations are presented in figs. 7 through 10, again at 10 μ sec which is long after the projectile stops. It is clear that the projectile deformation is reduced compared to our initial calculations. The calculated penetration depths for these calculations with improved material properties are compared to the experimental data in fig. 11. Agreement between the calculations and data is clearly improved and quite probably as good as can be expected in view of the scatter in the experimental data.

Summary:

We have determined material parameters that produce good agreement between the modeling calculations and the experimental data. However, the projectile steel is as yet uncharacterized so it is not possible to draw firm conclusions about the significance of the agreement between the calculated and measured projectile shapes. It would also be interesting to know whether the deduced polyethylene yield strength is consistent with the 1.5 kbar value we have adopted.

It is expected that more extensive comparisons will be done during face-to-face meeting with our French counterparts under the *aegis* of the ICF agreement. A proposed time for this phase of the work would be just prior to or subsequent to the Bordeaux ICF meeting this fall. Final plans for the report to satisfy the ICF-Agreement tasking will be made then. Additional experimental work and modeling tasks will also be discussed at that time.

References:

1. R. Courchinoux and A. Hereu, "Shrapnel generation and effects experiments at CESTA," presented at the LLNL/CEA meeting, September 22-26, 1997.
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3. Robert Tipton, "The CALE Code", LLNL Internal Report. See also Robert Tipton, "Modeling Flux Compression Generators with a 2D ALE Code," LLNL Internal Report UCRL 99900, November 1988.
4. A. Geille, private communication.
5. D. J. Steinberg, S. G. Cochran, and M. W. Guinan, "A Constitutive Model for Metals Applicable at High Strain Rates," J. Appl. Phys., 51, 1498 (1980). Updates to this EOS are found in Daniel J. Steinberg "Equation of State and Strength Properties of Selected Materials" Lawrence Livermore National Laboratory Report UCRL-MA-106439 change 1, February 13, 1996 and references contained therein.

Table 1

Material parameters for first calculations. Results are presented in figs. 2-6.

	Steel	Polyethylene
Equation of State	Gruneisen	Gruneisen
ρ	8.13 g/cm ³	0.957 g/cm ³
c	3980 m/s	3050 m/s
s ₁	1.58	1.328
s ₂	0	1.139
s ₃	0	-1.871
γ_0	1.6	0.67
a	0.5	0
ρ_{\min}	5.7 g/cm ³	0.48 g/cm ³
ρ_{\max}	20.6 g/cm ³	3.4 g/cm ³
Constitutive Model	Elastic-Plastic	Elastic-Plastic
G	641 kbar	50 kbar
Y	3 kbar	1 kbar
Damage Model	Spall	Spall
spall strength	20 kbar	20 kbar

Table 2

Calculated penetration depths at various incident velocities for steel projectile impinging normally on polyethylene

Incident velocity	LLNL Calculation (this work)	CEA Calculation (ref. 2)
<i>550 μm diameter projectile</i>		
0.35 km/s	0.48 mm	0.3 mm
0.85 km/s	1.50 mm	1.1 mm
1.10 km/s	2.08 mm	1.7 mm
<i>350 μm diameter projectile</i>		
1.2 km/s	1.40 mm	1.3 mm